



Article

Reduction of Heat Losses Using Quadruple Heating Pre-Insulated Networks: A Case Study

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Received: 25 October 2019; Accepted: 6 December 2019; Published: 10 December 2019



Abstract: The paper presents an analysis of heat loss and reductions of annual emissions of air pollutants of a quadruple pre-insulated heating network by comparing this solution with the existing pre-insulated network consisting of four pre-insulated single pipes and the variant consisting of two twin pipe pre-insulated. For calculations, an existing heating network located in central Poland was adopted, where heat is transported for heating purposes of buildings and domestic hot water with circulation of domestic hot water through four separate pre-insulated underground pipes. The idea of the construction of four pre-insulated pipes presented in the paper consists in the location of four steel pipes in a common round thermal insulation, which perform the role of heat transport for heating purposes in multi-family buildings (supply and return) and two pipes transporting hot water (a pipe with domestic hot water with circulation). In Poland, heating pipes used in multi-family housing have a larger diameter compared to domestic hot water pipes, which is why standard twin pipe heating pipes have been used in the construction of four pre-insulated networks, in which the domestic hot water pipe has been added to the thermal insulation and circulation of domestic hot water. In order to determine heat losses, a simplified two-dimensional model of conductive heat transfer was developed using Fortran to create a computer program. The results of numerical simulations show that the use of twin pipes for the construction of pre-insulated quadruple networks has contributed to a significant reduction in heat loss in relation to the existing single pre-insulated network (up to 57.1%), while reducing the thermal insulation field of the cross-section of the pre-insulated pipe by 21.4%.

Keywords: quadruple pipes; single pipes; twin pipes; pre-insulated district heating; network; energy savings; pollutants emission

1. Introduction

Energy-efficient operation of heating networks is primarily associated with the reduction of heat losses in pre-insulated pipes. The simplest method of reducing heat loss is to reduce the network operating temperature [1–5]. Unfortunately, the reduction of network operation parameters is associated with costly thermal modernization of the building, i.e., insulation of buildings and replacement of the heating system [6]. Reduction of heat loss in heating networks can also be achieved by using thicker layers of thermal insulation or heating networks with a lower thermal conduction coefficient of thermal insulation, which is associated with a higher cost of heating networks. Heat exchange in single pre-insulated heating networks, which are the most commonly used, has been thoroughly studied [7–11]. Heat losses in single pre-insulated pipes can be determined using analytical methods [3,7,9,12,13] as well as using numerical methods in two-dimensional [10,12] and three-dimensional [14] problems. Another method of reducing heat loss is to place a few pipes in common thermal insulation. This method is mainly used in twin pipes, where the supply and return

Energies **2019**, 12, 4699 2 of 12

pipes are located in circular insulation [15,16]. One of the methods to reduce heat loss in pre-insulated twin pipes is to change the cross-sectional shape of the twin pipe thermal insulation from round to oval [17], elliptical [18] or egg shape [19,20] while maintaining the same cross-sectional area of thermal insulation. Heat losses in pre-insulated twin pipes can be determined by simplified analytical methods [12,21,22] and numerical methods [16–19,23]. Heat losses in pre-insulated double pipes with round thermal insulation are about 30% lower than heat losses in pre-insulated single pipes [19,20,22]. It should be noted here that the improvement of thermal insulation also depends on the size of the pipes. In the case of double pre-insulated heating pipes with an egg-shaped cross-section, heat losses are smaller by about 45% compared to heat losses in single pre-insulated pipes [19,20]. The pre-insulated triple pipes are also described in the literature [15,19] in which heat is transported by means of two supply pipes and one return pipe.

Another alternative is pre-insulated quadruple pipes, where all four pipes are encased in common round thermal insulation. Pre-insulated quadruple ducts can be used for heat transport during the heating season and for the transport of domestic hot water along with the circulation of domestic hot water. While single pre-insulated and twin pipes have been thoroughly investigated [1–22], the heat loss analysis of four-pre-insulated pipes has not yet been performed.

The purpose of the work is to analyze heat loss and the ecological effect of pre-insulated quadruple pipes by comparing this solution with the existing pre-insulated network built of four single pre-insulated pipes and an additional adopted variant of the network consisting of two twin pipes. The reduction of heat loss is associated with lower emissions of pollutants into the air from heat sources if the heat source is fossil fuel, i.e., it significantly affects the ecological effect of heating networks operation [24,25]. The paper adopts the geometry of pre-insulated quadruple pipes by placing additional pipes for domestic hot water and circulation of domestic hot water in the thermal insulation of a standard twin pipe designed for heat transport for the purposes of heat demand of buildings.

2. Description of the Model for Determining Heat Loss in Pre-Insulated Quadruple Pipes

In order to determine heat losses through pre-insulated pipes, a computer program was created using the Fortran language using the boundary element method (BEM) [26], which is often used in many heat transfer analysis [27–29]. The boundary element method is a non-mesh method and for given boundary conditions in the form of temperature or heat flux, it allows the determination of heat fluxes for individual pipes inside thermal insulation. It should be noted that in the case of single heating networks and twin pipes, analytical formulas may be used to determine heat losses, the results of which are consistent with the results of numerical methods [12], while in the case of pre-insulated quadruple heating pipes in common thermal insulation, analytical formulas are not known. A two-dimensional simplified model of heat conduction described in Laplace's equation and the Fourier equations were used for calculations:

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0, \quad q_x = -\lambda \frac{\partial T}{\partial x}, \quad q_y = -\lambda \frac{\partial T}{\partial y}, \tag{1}$$

where T is the temperature, x and y are the coordinates of the Cartesian system in the cross section of the pre-insulated pipe, q_x and q_y are heat-flow quantities that are directed in the x and y directions, while λ is the thermal conductivity coefficient of the thermal insulation (polyurethane foam).

Figure 1 presents the boundary conditions of heat transfer using a simplified model of heat exchange inside a quadruple pre-insulated pipe. The Dirichlet boundary condition in the form of the external surface temperature of the thermal insulation $T_G = 8$ °C and the temperature of the walls of steel pipes equal to the temperature of the heating medium flowing on the T_S supply and return T_R as well as domestic hot water T_H together with the circulation of domestic hot water T_C was adopted for calculations. The thermal conductivity coefficient of thermally insulating materials depends on temperatures, material age and density. Standard thermal insulation made of polyurethane foam

Energies **2019**, 12, 4699 3 of 12

with an average thermal conductivity coefficient of $\lambda = 0.0265$ W/mK was used in the calculations. Parameters of thermal insulation made of polyurethane foam can be found in [30,31]. The unit heat losses q through the quadruple pre-insulated pipe consist of heat losses through the heating supply pipe q_S and return q_R and heat losses through the domestic hot water pipe q_H and domestic hot water circulation q_C :

$$q = q_S + q_R + q_H + q_C \tag{2}$$

where heat losses for individual pipes are described by the heat flux balance according to Figure 1:

$$q_R = q_{R2} - q_{R1} \tag{3}$$

$$q_H = q_{H3} - q_{H2} - q_{H1} \tag{4}$$

$$q_C = q_{C3} - q_{C2} - q_{C1} (5)$$

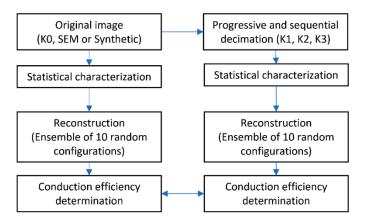


Figure 1. Geometry, boundary conditions and heat fluxes in pre-insulated quadruple pipes.

The solution of Equation (1) for given boundary conditions is the heat flux density at the boundary of thermal insulation. To determine heat loss by the boundary element method, no mesh inside the thermal insulation cross-section is required, only the boundary of the thermal insulation is discretized. After determining the heat flux density at the boundary of thermal insulation by the boundary element method, the temperature or density of the heat flux at any point within the cross-section of thermal insulation is also determined without the use of meshes. The computer program verification was carried out in the works [18,32]. A boundary of 5000 linear elements was used for calculations.

3. Analysis of Heat Losses of Pre-Insulated Quadruple Networks on the Basis of Operating Parameters of the Existing Pre-Insulated Single Network and the Adopted Twin Pipe Network

The analysis of quadruple pre-insulated network heat loss in a common thermal insulation was made on the basis of the operating parameters of the existing single pre-insulated network investment made in 2012, supplying heat from the local coal-fired heating plant during the heating season and domestic hot water for multi-family and service buildings located in central Poland. A satellite view of the housing estate of multi-family buildings connected to the heating network is shown in Figure 2a [33], while a diagram of the existing pre-insulated network with the diameters of single pre-insulated pipes is shown in Figure 2b.

Energies **2019**, 12, 4699 4 of 12

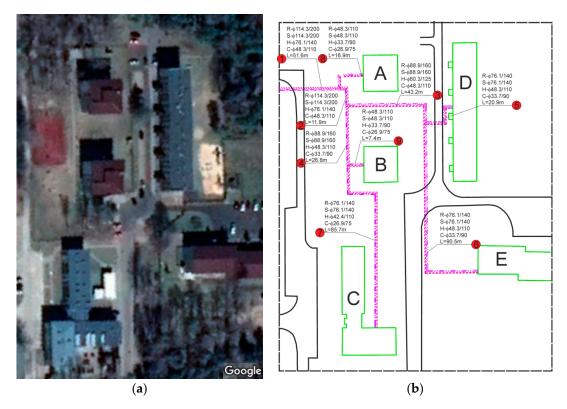


Figure 2. View of the analyzed housing estate from googlemaps.com [33] (a) and diagram (b) of an existing single heating network built of four separate pre-insulated pipes.

In order to analyze the energy losses for the purposes of heat loss and the ecological effect of the quadruple pre-insulated heating network, three variants of the pre-insulated network design were used for heating in the heating season and transporting hot water (Figure 3). The first variant marked as "I" is the existing state of a single pre-insulated network built of four pipes: the supply and return pipes of the heating system marked as S and R respectively (Figure 3a) and the pipe supplying domestic hot water to buildings and circulation of domestic hot water marked respectively as H and C (Figure 3a). Pre-insulated heating network pipes S and R with a flow temperature $T_S = 80$ °C and return temperature $T_R = 60$ °C work only during the heating season for a period of 255 days, while hot utility water pipes with a temperature T_H = 55 °C and T_C = 55 °C work all year round. The temperature of pre-insulated heating network, domestic hot water and circulation of domestic hot water is kept constant. The heating medium is transported through a pre-insulated network to local heating centers located in buildings, where behind the heat exchangers inside buildings the temperature of the heating medium is regulated depending on the outside temperature. Linear heat density for the analysed network was estimated at 3.3 MWh/(m year). Fluid flow was in a range from 1.58 t/h to 21.5 t/h in heating pipes and between 0.2 t/h and 0.45 t/h in hot water and circulation pipes. Loss of pressure for the design flow was 27.5 kPa and 5.0 kPa, respectively. The detailed geometry with the description of the pipe diameters and thermal insulation fields as well as the unit heat losses determined for the supply and return pipes of the existing heating network, respectively as q_{Ia} , q_{Ib} and the unit heat losses for existing domestic hot water pipes and domestic hot water circulation marked as q_{Ic} and q_{Id} , respectively, are presented in Table 1. The description of the geometric parameters from Table 1 is in Figure 3a.

Energies 2019, 12, 4699 5 of 12

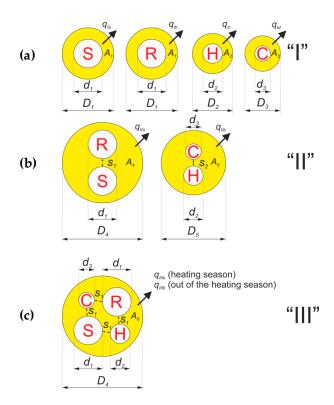


Figure 3. Variants of the analyzed heating network (A_i -area of thermal insulation; s_i -distance between pipes inside the thermal insulation; D_i , d_i - pipe diameters, and i-pipe numbers inside the thermal insulation): (a) variant I, (b) variant II and (c) variant III.

Table 1. Geometry of heating pipes of variant "I" (existing condition) with unit heat losses through single pre-insulated pipes.

No. Pipes	Supply Pipe				Retu	rn Pipe	n Pipe Hot Water Pipe			e	Circulation Pipe				Thermal Insulation Field		
(Figure 2b)	D_1	d_1	A_1	q_{Ia}	D_1	d_1	A_1	q_{Ib}	D_2	d_2	A_2	q_{Ic}	D_3	d_3	A_3	q_{Id}	$2 \times A_1 + A_2 + A_3$
	mm	mm	m ²	W/m	mm	mm	m ²	W/m	mm	mm	m ²	W/m	mm	mm	m ²	W/m	m ²
1,2	200	114.3	0.0212	21.4	200	114.3	0.0212	15.5	140	76.1	0.0108	19.7	110	48.3	0.0077	14.6	0.0608
3	160	88.9	0.0139	20.4	160	88.9	0.0139	14.7	125	60.3	0.0094	16.4	110	48.3	0.0077	14.6	0.0449
4	160	88.9	0.0139	20.4	160	88.9	0.0139	14.7	110	48.3	0.0077	14.6	90	33.7	0.0055	12.2	0.0409
5,6	140	76.1	0.0108	19.7	140	76.1	0.0108	14.2	110	48.3	0.0077	14.6	90	33.7	0.0055	12.2	0.0348
7	140	76.1	0.0108	19.7	140	76.1	0.0108	14.2	110	42.4	0.0081	12.6	75	26.9	0.0038	11.7	0.0336
8,9	110	48.3	0.0077	14.6	110	48.3	0.0077	10.5	90	33.7	0.0055	12.2	75	26.9	0.0038	11.7	0.0247

In the second variant (Figure 3b, Table 2) a heating network was adopted consisting of two twin pipe ducts working for heating purposes and domestic hot water on the same thermal parameters as in variant "I". The dimensions of the diameters of steel heating and domestic hot water were taken equal to the dimensions of the pipes in variant "I" and the standard diameters of thermal insulation were adopted. The geometry of the twin pipe ducts assumed for calculations (Figure 3b) and the determined unit heat losses of pre-insulated heating and domestic hot water pipes, q_{IIa} and q_{IIb} , respectively, are presented in Table 2.

Energies 2019, 12, 4699 6 of 12

Table 2. Geometry of heating and domestic hot water pipes variant "II" (two twin pipes) wit	n unit
heat losses.	

	Twin Pipe (Supply Pipe + Return Pipe)						Pipe (Ho	t Water I	Thermal Insulation			
No. Pipes	D_4	d_1	s_1	A_4	q_{IIa}	D_5	d_2	d_3	s_2	A_5	q_{IIb}	Field $A_4 + A_5$
(Figure 2b)	mm	mm	mm	m ²	W/m	mm	mm	mm	mm	m ²	W/m	m ²
1,2	315	114.3	25	0.0574	23.4	225	76.1	48.3	20	0.0270	11.4	0.0844
3	250	88.9	25	0.0367	24.0	200	60.3	48.3	20	0.0220	11.0	0.0587
4	250	88.9	25	0.0367	24.0	160	48.3	33.7	19	0.0147	10.6	0.0513
5,6	225	76.1	20	0.0307	20.6	160	48.3	33.7	19	0.0147	10.6	0.0453
7	225	76.1	20	0.0307	20.6	160	42.4	26.9	19	0.0161	8.8	0.0468
8,9	160	48.3	19	0.0164	17.5	140	33.7	26.9	19	0.0125	8.9	0.0289

The third variant (III) is a quadruple pre-insulated network, where two heat pipes and two domestic hot water pipes are located in one thermal insulation (Figure 3c, Table 3). Pre-insulated quadruple ducts have been designed using the assumed "II" heating ducts for twin pipe heating purposes. Figure 4a–d show an example of temperature and density distribution in a twin pipe, assuming $D_4 = 250$ mm and $d_1 = 88.9$ mm. Based on significant values of heat flux density (Figure 4b), local areas of significant intensification of heat exchange between the pipe and the environment and areas with low heat transfer, which are characterized by a low heat flux density, can be identified. Additional domestic hot water and domestic hot water circulation pipes can be placed in the area of thermal insulation where the heat flux density is low. The smallest heat flux density values are located on the left and right of the supply and return pipes (Figure 4b) and additional hot water pipes have been located here. It should be pointed out here that the pipes transporting domestic hot water used in Poland have smaller diameters than district heating pipes. The result of adding domestic hot water pipes and domestic hot water circulation is a reduction in the cross-sectional area of thermal insulation in pre-insulated quadruple pipes by about 40% compared to two twin pipes from variant II (Tables 1 and 3).

Table 3. Geometry of pre-insulated pipes of variant "III" (four pipes in common thermal insulation) and unit heat losses through quadruple pre-insulated pipes in the heating season q_{IIIa} and out of the heating season q_{IIIb} .

		Quadruple Pre-Insulated Pipe										
No. Pipes (Figure 1)	D_4	d ₁ (S,R)	d_2	d_3	s_1	Thermal Insulation Field A_6	Heating Season (S+R+H+C) q _{IIIa}	Out of the Heating Season (H+C) q _{IIIb}				
	mm	mm	mm	mm	mm	m ²	W/m	W/m				
1,2	315	114.3	76.1	48.3	25	0.0510	28.8	11.7				
3	250	88.9	60.3	48.3	25	0.0320	33.6	14.8				
4	250	88.9	48.3	33.7	25	0.0339	28.3	10.2				
5,6	225	76.1	48.3	33.7	20	0.0279	25.7	10.0				
7	225	76.1	42.4	26.9	20	0.0287	23.9	10.0				
8,9	160	48.3	33.7	26.9	19	0.0150	23.7	11.6				

Energies **2019**, 12, 4699 7 of 12

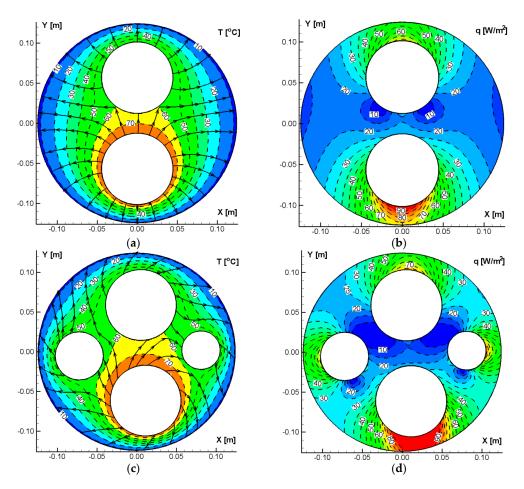


Figure 4. Temperature distribution with heatlines and heat flux density distribution for a twin pipe (a,b) and a quadruple pre-insulated pipes (c,d).

In quadruple pre-insulated pipes, an increase in the temperature gradient was observed (Figure 4c) as well as an increase in heat flux density (Figure 4d) inside the thermal insulation compared to twin pipes, however, the total heat loss of the quadruple pre-insulated network compared to two double-pre-insulated pipes are smaller. In order to reduce the heat exchange between four pipes in common thermal insulation, the minimum distances between these pipes s_1 (Table 3) have been adopted equal to the distances s_1 between pipes in twin pipe pre-insulated pipes (Table 4). The impact of distance between heating pipes on heat losses of pre-insulated pipes has been described in papers [15,18,19]. By analysing heat exchange in pre-insulated pipes, it is also possible to reduce heat losses by modifying the shape of thermal insulation, which was also done in works for twin pipe pre-insulated pipes [17,20].

In order to analyze the thermal insulation of the quadruple heating pre-insulated network, energy for heat losses was determined for the existing condition of the pre-insulated network and for two assumed variants. Energy for heat losses on individual sections of pre-insulated pipes was determined in accordance with the following relationship:

$$E_i = \sum_{j=1}^{N} q_{ji} L_j t \tag{6}$$

where j is the pipe number according to Figure 2b and Tables 1–3, L_i is the length of the pipe according to Figure 2b, t is time, q_{ji} is the unit heat loss depending on the adopted variant, N- total number of pipes, which is described by the relationships in Table 4 and the unit heat loss values from Tables 1–3, while the lower index i is the type of variant (i = I, II, III).

Energies **2019**, 12, 4699 8 of 12

Unit Heat Losses During the Heating Season	Unit Heat Losses in the Off-Heating Season
Case	I
$q_{Ij} = q_{Ia} + q_{Ib} + q_{Ic} + q_{Id}$	$q_{Ij} = q_{Ic} + q_{Id}$
Case	II
$q_{IIj} = q_{IIa}$	$q_{IIj} = q_{IIb}$
Case 1	II
$q_{IIIj} = q_{IIIa}$	$q_{IIIj} = q_{IIIb}$

Table 4. Formulas describing unit heat losses for the adopted variants.

Table 5 shows energy consumption for heat losses for three heating network variants (I, II, III) detailing the heating season (255 days), non-heating season (110 days), when the network only transports domestic hot water with circulation and annual energy consumption for heat losses (365 days).

Heating Network Variant	Energy Consumed for Heat Losses During the Heating Season (255 Days) [GJ]	Energy Consumed for Heat Losses in the Off-Heating Season (110 Days) [GJ]	Annual Energy Consumed for Heat Losses (365 Days) [GJ]
Pre-insulated single heating network, current condition (S, R, H, C), Case I	493.7	95.9	589.6
Two pre-insulated twin pipe heating networks (S + R, H + C), Case II	254	35.3	289.3
Quadruple heating pre-insulated network (S + R + H + C), Case III	214.7	38.2	252.8

Table 5. Energy for heat losses for the three variants adopted.

Figure 5a presents the percentage comparison of the cross-sectional area of thermal insulation of selected pre-insulated pipes, while Figure 5b presents the percentage comparison of the annual energy consumption for heat losses of selected pipes, assuming that the existing condition (variant I) is equal to 100% both in the case of surface area thermal insulation and energy consumption for heat losses.

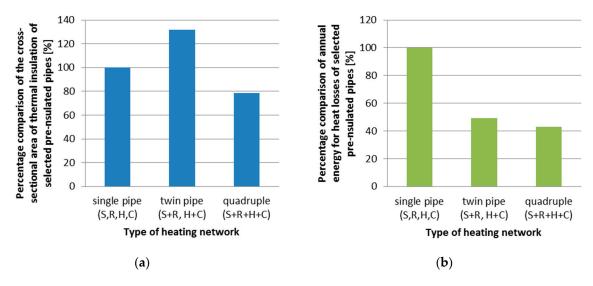


Figure 5. Percentage comparison of the cross-sectional area of thermal insulation (**a**) and annual energy for heat loss (**b**) assuming that variant I is equal to 100%.

Energies **2019**, 12, 4699 9 of 12

Annual energy consumption for heat losses in quadruple networks (variant III) is about 57.1% and 12.6% (Table 5) lower than for four single pre-insulated networks (variant I) and two double pre-insulated networks (variant II) respectively. It should be noted here that the average surface area of thermal insulation in adopted quadruple pre-insulated heating networks is lower by 21.4% and 40.2%, respectively, than four single pre-insulated networks and two double pre-insulated networks.

The main assumption of this work was the use of pre-insulated double thermal insulation for the construction of quadruple pipes by adding two domestic hot water pipes to twin pipe heating pipes in common thermal insulation, therefore it was not decided to increase the surface area of thermal insulation in quadruple pipes. In the case of increasing the surface area of thermal insulation of quadruple pipes (variant III) to the value of the field of thermal insulation of double pre-insulated pipes (variant II), the heat loss of the quadruple pipe in relation to two double pipes would be much smaller. The largest area of thermal insulation in the cross-section of pre-insulated pipe has two double pre-insulated networks in which the insulation area is 31.1% larger (Figure 5a) than the insulation field for four single pre-insulated networks (variant I), resulting in annual energy (Figure 5b) for heat losses of two twin pipe pre-insulated pipes (variant II) is about 51% smaller than in variant I.

Analysing the unit heat losses in the heating season without taking into account the domestic hot water, it can be seen that in the case of twin pipes the unit heat losses (Table 2) are smaller by about 34.8% than single pre-insulated networks (Table 1). Similar results were obtained in [19,20,22] (Figure 6), where the differences between the results did not exceed 5%. After taking into account the heat losses in domestic hot water pipes and circulation of domestic hot water, the unit heat losses in twin pipes are lower by as much as 50% from the unit heat losses of single pre-insulated pipes. Such a significant difference in unit heat losses between twin pipes and single pipes, including hot water pipes, results from the fact that hot water pipes and hot water circulation pipes are characterized by small diameters, which are much better thermally insulated than single pre-insulated pipes for these small diameters.

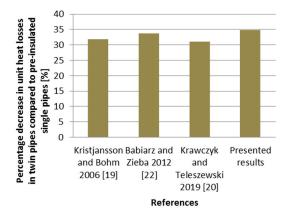


Figure 6. Percentage decrease in unit heat losses in twin pipe heating pipes without taking into account hot water pipes compared to single pre-insulated pipes.

In the period outside the heating season, when the network only transports domestic hot water (Table 5), energy for heat losses in pre-insulated quadruple pipes is slightly higher than in the case of two double pre-insulated pipes, which is caused by a smaller thickness of thermal insulation in pre-insulated quadruples relative to twin pipe hot water.

Based on the determined annual energy for heat losses and emissivity coefficients [34,35], the ecological effect of using pre-insulated quadruple pipes for the following pollutants emitted into the atmosphere was determined: nitrogen oxides (NOX), carbon monoxide (CO), non-methane volatile organic compounds (NMVOC), sulfur oxides (SOX), total suspended particles (TSP), particulate matter (PM10 and PM2.5), carbon dioxide (CO2) and methane (CH4). Reductions of annual emissions of air pollutants for all variants were determined using the known formula [34]:

Energies **2019**, 12, 4699

$$\Delta E_{I-i} = (E_I - E_i) \times E_f \tag{7}$$

where: E_I is the annual energy for heat losses in the existing variant of type I, (single four-pipe network), while E_I (i = II or i = III) is the annual energy for heat losses in variants II and III. Annual energy for the purposes of heat losses E_I , E_{II} and E_{III} are determined from formula 6.

As showed in Table 6, the average annual emission of pollutants for variant III (quadruple pre-insulated network) is lower by approximately 57% and 13% compared to the condition of the existing variant I (single pre-insulated network) and two twin pipe ducts (variant II), respectively. It should be noted here that pollutants emitted to the atmosphere as a result of fuel combustion depend on the composition of the fuel and the method of combustion.

Pollutant	$E_f[g/GJ]$	$E_I E_f$ [kg/year]	$E_{II}E_f$ [kg/year]	$E_{III}E_f$ [kg/year]	ΔΕ _{Ι-ΙΙ} [kg/year]	ΔΕ _{Ι-ΙΙΙ} [kg/year]
NO _x	209.0	123.2	60.5	52.8	62.8	70.4
CO	8.7	5.130	2.517	2.200	2.612	2.930
NMVOC	1.0	0.590	0.289	0.253	0.300	0.337
SO_x	820	483.5	237.3	207.3	246.2	276.2
TSP	11.4	6.722	3.298	2.882	3.423	3.839
PM10	7.7	4.540	2.228	1.947	2.312	2.593
PM2.5	3.4	2.005	0.984	0.860	1.021	1.145
CO_2	98,300	57,960.0	28,442.3	24,854.2	29,517.7	33,105.8
CH_4	1	0.590	0.289	0.253	0.300	0.337

Table 6. Annual pollutant emissions determined for variants I, II and III.

4. Conclusions

Standard thermal insulation in twin pipe ducts used for heat transport allows the placement of two additional smaller diameter pipes compared to heating pipes. Such pipes can be domestic hot water pipes and domestic hot water circulation pipe, which together with the heating pipes form a pre-insulated quadruple pipe. Quadruple pre-insulated pipes significantly reduce heat loss and increase the ecological effect compared to four single pre-insulated pipes while reducing the cross-sectional area of the thermal insulation. An additional advantage is the smaller trench in the ground for a pre-insulated quadruple pipes compared to four single or two pre-insulated double pipes. The presented solution of pre-insulated quadruple pipes can also be an alternative to two twin pipes, where one pre-insulated double pipe is transported heat, while the other twin pipe is used for domestic hot water along with the circulation of domestic hot water. Comparing the pre-insulated quadruple pipes with two twin pipes, also smaller heat losses and smaller thermal insulation field in the cross-section of the pipes were obtained.

Author Contributions: D.A.K. and T.J.T. proposed the research methodology and aims, as well as organized the draft of the manuscript; T.J.T. conducted simulations and prepared figures, D.A.K., T.J.T. and A.R. analyzed the simulation results, wrote the manuscript and agreed to submission.

Funding: This research was funded by NAWA, BUT InterAcademic Partnerships (PPI/APM/2018/1/00033/DEC/1) and WZ/WBiIS/9/2019 scientific research at Bialystok University of Technology.

Conflicts of Interest: The authors declare no conflict of interest.

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Energies **2019**, 12, 4699 11 of 12

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